

DESCRIPTION

A SAWTOOTH WAVE GENERATING APPARATUS,
A METHOD OF GENERATING SAWTOOTH WAVE, A CONSTANT CURRENT CIRCUIT,
AND A METHOD OF ADJUSTING AMOUNT OF CURRENT FROM THE SAME

Technical Field

The present invention relates to a sawtooth wave generating apparatus, a method of generating sawtooth wave, a constant current circuit, and a method of adjusting the amount of current from the same, more particularly, to such an apparatus and a method which are used in a PWM driving device, a PWM display device, or the like.

Background Art

In a conventional sawtooth wave generating apparatus, a signal having a desired reference frequency is generated using a fixed oscillation frequency of an oscillator such as a crystal oscillator, and then a sawtooth wave is generated using the signal having the desired reference frequency. The structure of a conventional sawtooth wave generating apparatus will be described with reference to Figs. 9 and 10.

Fig. 9 is a schematic block diagram of a conventional sawtooth wave generating apparatus 2. As shown in Fig. 9, the conventional sawtooth wave generating apparatus 2 includes a fixed frequency generating section 3 for generating a reference frequency fixed at a predetermined value using a crystal oscillator or the like, and a sawtooth wave generating section 4 for generating a sawtooth wave based on the reference frequency. In this way, since using a piezoelectric element or the like having a piezoelectric effect as a load, i.e., driving a load whose resonant point is changeable was not taken into consideration, such the fixed frequency generating section 3 has been utilized.

Fig. 10 is a circuit diagram illustrating an example of the circuit structure of the sawtooth wave generating section 4 shown in Fig. 9. As shown in Fig. 10, the sawtooth wave generating

section 4 includes a variable resistor 4R whose resistive value can be changed manually, and a plurality of capacitors 4C each having a predetermined capacitance, one of which can be set (selected). In this case, in the sawtooth wave generating section 4 shown in Fig. 10, the shape of the sawtooth wave including a slope of the sawtooth wave is changeable by changing the resistive value of the variable resistor 4R, and the cycle of the sawtooth wave (the period between a rising edge and trailing edge of the sawtooth wave) is changeable by selecting one capacitor within the plurality of capacitors 4C.

The generated sawtooth wave is utilized in an apparatus carrying out the PWM control such as a PWM driving device or a PWM display device as disclosed in, for example, Japanese Laid-Open Patent Application No. HEI. 11-180529. The PWM control is one in which a signal having a predetermined duty ratio for controlling the drive of each of various devices is utilized to control ON/OFF of the device by comparing a predetermined voltage value with the voltage value of the sawtooth wave (voltage waveform) by means of a voltage comparator.

Further, in Japanese Laid-Open Patent Application No. HEI. 11-180529, a method of controlling the drive of elliptic-oscillation parts feeder using a resonant frequency is disclosed in which the resonant point is track-controlled using a variable frequency power supply.

However, in the conventional sawtooth wave generating apparatus 2, in the case where the PWM control is carried out in a driving device using the resonant point of a resonant device, a clear (or stable) sawtooth wave could not be formed because the resonant frequency is changeable.

Namely, the sawtooth wave generated from the resonant frequency of a resonant driving device was utilized in the PWM control. However, since the resonant frequency was changeable, the PWM control could not be stabilized at a predetermined duty

ratio. Thus, there is a problem that the duty ratio is changed constantly in such a case.

Further, there is another problem that a stable sawtooth wave having a certain shape cannot be formed which becomes a reference signal of the PWM control because the resonant frequency for the PWM control is changed constantly.

Disclosure of Invention

In view of the above-mentioned problems of the prior art, it is therefore an object of the present invention to provide a sawtooth wave generating apparatus and a method of generating a sawtooth wave that can stably supply a sawtooth wave in response to variation in a resonant frequency in the case of PWM-controlling a driving device with a piezoelectric element whose resonant frequency constantly undergoes a change, or carrying out the PWM control by arbitrarily changing the resonant frequency.

In order to achieve the above object, in one aspect of the present invention, the present invention is directed to a sawtooth wave generating apparatus that can generate a sawtooth wave stably. The sawtooth wave generating apparatus comprises:

a reference signal generating section for generating a reference signal having a predetermined frequency;

a sawtooth wave forming section which forms a sawtooth wave based on the predetermined frequency of the reference signal generated by the reference signal generating section; and

a correcting section which automatically corrects a slope of the sawtooth wave defined by $\Delta V/t$ which is formed by the sawtooth wave forming section in response to variation of the predetermined frequency of the reference signal.

In the sawtooth wave generating apparatus of the present invention, the reference signal having the predetermined frequency is generated by the reference signal generating section, the sawtooth wave is formed by the sawtooth wave forming section based on the predetermined frequency, and then the slope of the formed

sawtooth wave, i.e., the value $\Delta V/t$ is automatically corrected by the correcting section. Thus, according to the sawtooth wave generating apparatus of the present invention, it is possible to stably supply a sawtooth wave in response to variation in a resonant frequency in the case of PWM-controlling a driving device with a piezoelectric element whose resonant frequency constantly undergoes a change, or carrying out the PWM control by arbitrarily changing the resonant frequency.

In this case, it is preferred that the reference signal is a square-wave having rising edges and trailing edges, and the correcting section comprises:

a voltage comparator which compares the voltage of the sawtooth wave formed by the sawtooth wave forming section with a predetermined voltage;

a phase comparator which compares the phase of the rising edge of the reference signal generated by the reference signal generating section with the phase of the output signal from the voltage comparator; and

a low-pass filter which cuts out a high frequency component of the output signal from the phase comparator, and feeds back the resulting output signal to the sawtooth wave forming section.

Further, it is preferred that the phase comparator outputs a low-level signal so as to make the value $\Delta V/t$ smaller in the case where the phase of the output signal from the voltage comparator is earlier than the phase of the rising edge of the reference signal, and the phase comparator outputs a high-level signal so as to make the value $\Delta V/t$ larger in the case where the phase of the output signal from the voltage comparator is later than the phase of the rising edge of the reference signal.

Moreover, it is preferred that the reference signal generating section includes a base frequency generating section comprising a PLL circuit, and a frequency generating section for generating the reference signal based on the output signal from the base frequency generating section.

Further, it is preferred that the sawtooth wave forming section includes a constant current circuit which outputs a constant current, a capacitor which is charged by the output current from the constant current circuit, and a semiconductor device for discharging the electric charge stored in the capacitor.

In this case, it is preferred that the semiconductor device includes an IGFET.

Further, it is preferred that the sawtooth wave generating apparatus further comprises a sawtooth wave discharging pulse section which controls discharge timing of the electric charge stored in the capacitor by outputting an on/off signal for the semiconductor device based on the output signal from the voltage comparator.

Moreover, it is preferred that the constant current circuit is capable of controlling the amount of the output current based on the output signal from the low-pass filter.

Further, it is preferred that the constant current circuit comprises a constant voltage source which outputs a constant voltage, a second FET for using a constant current characteristic of drain current, and a first FET for controlling the drain current of the second FET, a source electrode of the first FET being connected to a source electrode of the second FET;

wherein a gate electrode of the first FET is connected to the output side of the low-pass filter to control the amount of the output current from the constant current circuit, and both a gate electrode of the second FET and a drain electrode of the first FET are connected to the constant voltage source.

Further, in another aspect of the present invention, the present invention is directed to a method of generating a sawtooth wave. The method comprises the steps of:

generating a reference signal having a predetermined

frequency, the reference signal being a square-wave having rising edges and trailing edges;

forming a sawtooth wave based on the generated reference signal;

comparing the phase of the rising edge of the reference signal with the phase of the apex of the formed sawtooth wave; and

automatically correcting a slope of the sawtooth wave defined by $\Delta V/t$ based on the result of the phase comparison.

In this case, it is preferred that the automatically correcting step comprises:

generating a pulse signal when the voltage value of the sawtooth wave reaches a predetermined voltage value;

comparing the phase of the pulse signal with the phase of the rising edge of the reference signal; and

correcting the slope of the sawtooth wave so as to make the value $\Delta V/t$ smaller in the case where the phase of the pulse signal is earlier than the phase of the rising edge of the reference signal, and to make the value $\Delta V/t$ larger in the case where the phase of the pulse signal is later than the phase of the rising edge of the reference signal.

Further, in yet another aspect of the present invention, the present invention is directed to a constant current circuit which outputs a constant current. In this regard, a current control device which resides outside of the constant current circuit is capable of controlling the amount of the output current of the constant current circuit. The constant current circuit comprises:

a constant voltage source capable of outputting a constant voltage;

a second FET, a gate electrode of the second FET being connected to the output side of the constant voltage source, and a drain electrode of the second FET constituting an output terminal of the constant current circuit; and

a first FET capable of controlling the amount of the output current from the drain electrode of the second FET based on a control

signal inputted from the current control device, a drain electrode of the first FET being connected to the constant voltage source and a gate electrode of the second FET, and a gate electrode of the first FET being connected to the current control device.

In this case, it is preferred that the current control device includes a low-pass filter, and the control signal is a variable voltage signal to make the constant current circuit output a desired amount of current as the drain current of the second FET.

Moreover, in yet another aspect of the present invention, the present invention is directed to a method of adjusting the amount of an output current from a constant current circuit. In this regard, the constant current circuit includes a constant voltage source capable of outputting a constant voltage, a first FET, and a second FET. The method comprises:

adjusting the amount of a drain current of the second FET by changing the voltage applied to a gate electrode of the first FET, thereby changing the amount of the output current of the constant current circuit corresponding to the amount of the drain current.

Brief Description of Drawings

The foregoing and other objects, features and advantages of the invention will become more readily apparent from the following detailed description of a preferred embodiment of the invention which proceeds with reference to the accompanying drawings.

Fig. 1 is a schematic block diagram illustrating a main portion (circuit diagram) of a sawtooth wave generating apparatus according to the present invention.

Fig. 2 is a block diagram schematically illustrating a base frequency generating section in the sawtooth wave generating apparatus shown in Fig. 1.

Fig. 3 is a block diagram schematically illustrating a frequency generating section in the sawtooth wave generating apparatus shown in Fig. 1.

Fig. 4 is a block diagram schematically illustrating a sawtooth wave forming section in the sawtooth wave generating apparatus shown in Fig. 1.

Fig. 5 is a block diagram schematically illustrating a sawtooth wave discharging pulse circuit in the sawtooth wave generating apparatus shown in Fig. 1.

Fig. 6 shows timing charts schematically illustrating output signals from the base frequency generating section, the frequency generating section and the sawtooth wave discharging pulse circuit in the sawtooth wave generating apparatus shown in Fig. 1, and an output signal from the sawtooth wave generating apparatus shown in Fig. 1.

Fig. 7 shows timing charts schematically illustrating output signals from a voltage comparator and a phase comparator, which correspond to enlarged view of the timing charts shown in Fig. 6.

Fig. 8 is a graph illustrating a resonant frequency characteristic of a piezoelectric element.

Fig. 9 is a schematic block diagram of a conventional sawtooth wave generating apparatus.

Fig. 10 is a circuit diagram illustrating an example of the circuit structure of a sawtooth wave generating section shown in Fig. 9.

Best Mode for Carrying Out the Invention

A detailed description of the preferred embodiments of a sawtooth wave generating apparatus and a method of generating a sawtooth wave according to the present invention will now be made with reference to Figs. 1-8. Now, it should be noted that the embodiments (disclosure) are to be considered as an exemplification, and therefore this feature should not be intended to limit the present invention to the specific embodiments illustrated.

First, a description will be given for the structure of a sawtooth wave generating apparatus 1 of the present invention. Fig. 1 is a schematic block diagram illustrating a main portion (circuit diagram) of a sawtooth wave generating apparatus 1 according to

Fig. 5 is a diagram illustrating the relationship between the duty ratio controlled by the duty control section and the phase comparing position determined by the phase reference forming section.

Fig. 6 is a diagram schematically illustrating an example of a circuitry of the driver shown in Fig. 1.

Fig. 7 is a diagram schematically illustrating waveforms of signals in the case where a drive analog control signal to be supplied to drive the piezoelectric load is one whose output is raised to a predetermined output level at a given rate.

Figs. 8(A) and 8(B) are diagrams illustrating the structures in which two vibrating elements each including a piezoelectric element that is controlled by the resonance control apparatus according to the present invention rotate a rotor.

Fig. 9 is a diagram illustrating the partial structure of the resonance control apparatus according to the present invention in the case of using the two vibrating elements shown in Fig. 8(A).

Fig. 10 is a diagram illustrating waveforms of the signals for normal drive and reverse drive respectively controlled by normal-driving and reverse-driving duty control sections in response to a reference signal.

Fig. 11 is a block diagram schematically illustrating a main portion of a conventional resonance control apparatus.

Best Mode for Carrying Out the Invention

A detailed description of the preferred embodiments of a resonance control apparatus and a method of controlling a resonant device according to the present invention will now be made with reference to Figs. 1-10. Now, it should be noted that the embodiments (disclosure) are to be considered as an exemplification, and therefore this feature should not be intended to limit the present invention to the specific embodiments illustrated.

First, a description will be given for the structure of the resonance control apparatus 100 of the present invention. Fig. 1 is a schematic block diagram illustrating a main portion (circuit

diagram) of the resonance control apparatus 100 according to the present invention. As shown in Fig. 1, the resonance control apparatus 100 includes a voltage controlled oscillator (VCO) 10, a divider 20, a duty control section 30, a voltage comparator 40, a phase reference forming section 50, a first phase correction section (phase correction A) 51, a second phase correction section (phase correction B) 52, a phase comparator 60, a low-pass filter (LPF) 70, a driver 80, and a reference voltage setting section 90 for setting a voltage value that is a reference voltage for the voltage comparator 40. In this regard, a piezoelectric load (resonant device) 3 whose drive is controlled by means of the resonance control apparatus 100 is connected to the driver 80, and a piezoelectric sensor (resonant sensor) 2 for detecting the driving state of the piezoelectric load 3 in synchronization with the driving of the piezoelectric load 3 is connected to one input terminal of the voltage comparator 40. A detailed description of each component is given below. In this case, as shown in Fig. 1, a central processing unit (CPU) 1 controls the divider 20, the duty control section 30, the phase reference forming section 50, the first phase correction section 51, and the second phase correction section 52.

The VCO 10 generates a reference signal having a predetermined frequency based on the output signal (voltage signal) from the phase comparator 60 described later whose high frequency component is cut out by the LPF 70, and outputs the reference signal. The output signal from the VCO 10 is inputted to the divider 20, the duty control section 30, the phase reference forming section 50, and the first phase correction section 51.

The divider 20 divides the frequency of the reference signal that is the output signal from the VCO 10 by a predetermined value. The output signal from the divider 20 whose frequency is divided is inputted to the phase reference forming section 50, and the second phase correction section 52. In this regard, the dividing ratio of the divider 20 is controlled by the CPU 1.

The duty control section 30 controls a duty ratio of a drive signal for the piezoelectric load 3 by control of the CPU 1. The output signal from the duty control section 30 is inputted to the second phase correction section 52. The second phase correction section 52 controls the setting of the duty ratio of the output signal from the divider 20 based on a control signal inputted from the duty control section 30 to output the signal (this is the drive signal) to the driver 80. Then, the driver 80 inputs the drive signal to the piezoelectric load 3 to control the driving of the piezoelectric load 3. In this regard, the relationship between the duty ratio and drive vector ratio of the piezoelectric load (piezoelectric element) 3 will be described later (see Fig. 4).

The piezoelectric sensor 2 detects the driving state of the piezoelectric load 3 in synchronization with the driving of the piezoelectric load 3. The detected signal (voltage signal) that is the output signal from the piezoelectric sensor 2 is inputted to one input terminal of the voltage comparator 40. Further, a voltage signal that is the reference for voltage comparison in the voltage comparator 40 is set by the reference voltage setting section 90 to input the reference voltage to the other input terminal of the voltage comparator 40. In this case, in the present embodiment, the reference voltage setting section 90 is consisted of two resistors or variable resistors and a constant voltage source. The voltage value of the reference voltage signal may be set manually in the case where the reference voltage setting section 90 includes one or two variable resistor(s). However, the present invention is not limited to this structure. For example, the voltage value may be controllable by the CPU 1. The voltage value of the reference voltage signal (this is a predetermined voltage value, i.e., threshold for the voltage comparison) is previously set based on the resonant frequency characteristic of the piezoelectric load 3 to be utilized. The detailed description thereof will be described later.

The voltage comparator 40 compares the output signal from the piezoelectric sensor 2 (i.e., detected signal) with the

reference voltage signal. Then, in the case where the voltage value of the output signal from the piezoelectric sensor 2 is larger than the voltage value of the reference voltage signal, the voltage comparator 40 outputs a high-level signal to the first phase correction section 51. On the other hand, in the case where the voltage value of the output signal is smaller than the voltage value of the reference voltage signal, the voltage comparator 40 outputs a low-level signal to the first phase correction section 51. Namely, the voltage comparator 40 digitizes the output signal from the piezoelectric sensor 2 to output the digitized signal (i.e., high-level or low-level signal) to the first phase correction section 51.

The phase reference forming section 50 delays the phase of the output signal from the divider 20 for a predetermined interval (time), and selects either a rising edge or a trailing edge of the delayed signal based on the duty ratio of the drive signal controlled by the CPU 1 and the duty control section 30. The delayed signal outputted from the phase reference forming section 50 is inputted to one input terminal of the phase comparator 60. In this regard, the operation of the phase reference forming section 50 will be described later.

The first phase correction section 51 delays the phase of the voltage comparison signal inputted from the voltage comparator 40 by control of the CPU 1. The delayed signal outputted from the first phase correction section 51 is inputted to the other input terminal of the phase comparator 60. In this way, since the resonance control apparatus 100 can delay the phase of each of the signals inputted to the phase comparator 60 via the two input terminals thereof by means of the phase reference forming section 50 and the first phase correction section 51, the signal inputted from the phase reference forming section 50 can be also adjusted so that the inputted signal is apparently led.

The phase comparator 60 compares the phase of the signal inputted from the first phase correction section 51 with the phase

duration when the output signal remains the high level, and accordingly the drain current flowing between the source and drain electrodes of the second FET 302 is increased. On the other hand, in the case where the output signal from the LPF 80 is a low level, the voltage applied to the gate electrode of the first FET 301 is decreased according to the duration when the output signal remains the low level, and accordingly the drain current flowing between the source and drain electrodes of the second FET 302 is decreased.

The IGFET 305 is on/off-controlled based on the output signal from the sawtooth wave discharging pulse circuit 40, which is connected to a gate electrode of the IGFET 305. When the IGFET 305 is turned off, i.e., when the drain current of the IGFET 305 does not flow, the constant current flows from the constant current circuit 310 to the capacitor 304, thereby charging the capacitor 304 linearly. The electric charge Q stored in the capacitor 304 is indicated by the current I_D times time t . The potential difference between the conducting surfaces of the capacitor 304, which is indicated by Q/C (where C is a capacitance of the capacitor 304), becomes an output signal from the sawtooth wave forming section 30, and then a line having a slope defined by $\Delta V/t$ that is a part of the sawtooth wave is formed based on this output signal.

When the IGFET 305 is turned on after the elapse of a predetermined time, the electric charge stored in the capacitor 304 is instantaneously discharged through the resistor 303 and the IGFET 305 (where a discharge current is $I_{\text{discharge}}$), and then the output signal (voltage signal) becomes zero. By repeating this process periodically, the output signal of a sawtooth wave is formed in the sawtooth wave forming section 30. The formed sawtooth wave is outputted to the amplifier 50, and amplified by the amplifier 50. The amplified sawtooth wave becomes an output signal of the sawtooth wave generating apparatus 1, i.e., a sawtooth wave output signal.

The voltage comparator 60 compares the voltage of the output signal (voltage signal) from the amplifier 50 (i.e., the voltage

of a sawtooth wave output voltage signal) with the voltage of an output signal from the DAC 91 (i.e., the voltage of a given voltage signal). When the sawtooth wave output voltage signal is larger than the given voltage signal, the voltage comparator 60 outputs a high-level signal to the sawtooth wave discharging pulse circuit 40 and the phase comparator 70.

Fig. 5 is a block diagram schematically illustrating a sawtooth wave discharging pulse circuit 40 in the sawtooth wave generating apparatus 1 shown in Fig. 1. As shown in Fig. 5, the sawtooth wave discharging pulse circuit 40 includes a edge storing section 401, a delay circuit 402, and an AND circuit 403 which carries out the logical multiplication of the output signal from the edge storing section 401 and the inverted output signal of the delay circuit 402. The sawtooth wave discharging pulse circuit 40 outputs a signal for forming the edge of the sawtooth wave to be formed in the sawtooth wave forming section 30 to the sawtooth wave forming section 30 in response to the output signal from the voltage comparator 60.

To be more precise, when the output signal from the voltage comparator 60 is a high level, i.e., when the sawtooth wave output signal (voltage signal) reaches over the predetermined voltage value, the edge storing section 401 into which the high-level signal is inputted holds the high-level signal to output the signal to both the delay circuit 402 and the AND circuit 403 using the output signal from the base frequency generating section 10 as a clock signal (see Fig. 1). The delay circuit 402 delays the inputted signal for a predetermined time to output the delayed signal to the AND circuit 403. Then, the AND circuit 403 carries out the logical multiplication of the output signal from the edge storing section 401 and the inverted output signal of the delay circuit 402 to output a pulse signal each pulse having a width corresponding to the predetermined time to the sawtooth wave forming section 30. Namely, the pulse signal is the output signal from the sawtooth wave discharging pulse circuit 40.

The phase comparator 70 compares the phase of a rising edge of the reference signal outputted from the frequency generating section 20 with the phase of a voltage comparison signal outputted from the voltage comparator 60. The phase comparator 70 outputs a low-level signal to the LPF 80 for the time corresponding to the phase delay between the two signals in the case where the frequency of the voltage comparison signal is higher than the frequency of the reference signal. On the other hand, the phase comparator 70 outputs a high-level signal to the LPF 80 for the time corresponding to the phase lead between the two signals in the case where the frequency of the voltage comparison signal is lower than the frequency of the reference signal.

The LPF 80 cuts out a high frequency component of the output signal from the phase comparator 70, and outputs (feeds back) the resulting output signal to the gate electrode of the first FET 301 in the sawtooth wave forming section 30 as mentioned above.

In this regard, the base frequency generating section 10 and the frequency generating section 20 constitute a reference signal generating section, and the voltage comparator 60, the phase comparator 70 and the LPF 80 constitute a correcting section.

Next, a description will be given for the operation of the sawtooth wave generating apparatus 1 of the present invention with reference to timing charts of Figs. 6 and 7. Fig. 6 shows timing charts schematically illustrating output signals from the base frequency generating section 10, the frequency generating section 20 and the sawtooth wave discharging pulse circuit 40 in the sawtooth wave generating apparatus 1 shown in Fig. 1, and an output signal from the sawtooth wave generating apparatus 1 shown in Fig. 1.

In the timing charts shown in Fig. 6, from the top of the figure, an output signal from the base frequency generating section 10 (see Fig. 6(A)), an output signal from the frequency generating section 20 (i.e., the reference signal) (see Fig. 6(B)), an output

signal from the sawtooth wave discharging pulse circuit 40 (see Fig. 6(C)), and three patterns of an output signal from the sawtooth wave forming section 30 (i.e., the sawtooth wave output signal) (see Figs. 6(D)-6(F)) are illustrated.

In this case, the three patterns illustrated in Figs. 6(D)-6(F) respectively correspond to the case where a current value that is inputted to the capacitor 304 from the constant current circuit 310 is larger than a predetermined value, the case where the current value is smaller than the predetermined value, and the case where the current value is substantially equal to the predetermined value. In the case where the current value is equal to the predetermined value, the sawtooth wave is optimally formed.

As shown in these timing charts, the output signal from the sawtooth wave discharging pulse circuit 40 includes pulses in synchronization with the rising edges of a square-wave that is the output signal from the frequency generating section 20. Further, in synchronization with the pulse signal, the electrical charge stored in the capacitor 304 in the sawtooth wave forming section 30 is discharged, whereby the sawtooth wave output signal that is the output signal from the sawtooth wave forming section 30 is sharply fallen to its original state (namely, the voltage of the output signal becomes zero).

Further, as shown in Fig. 6(D), in the case where the output current value of the constant current circuit 310 is larger than the predetermined value, the amount of current flowing into the capacitor 304 becomes large, thereby making the slope of the sawtooth wave large, i.e., making the value $\Delta V/t$ larger (than the present value). Thus, the formed sawtooth wave increases at the timing earlier than a predetermined timing (i.e., the timing of the rising of the output signal from the frequency generating section 20) by rapidly charging the capacitor 304 in the sawtooth wave forming section 30, and then keeps at a substantially constant value (i.e., the output voltage value of the voltage source 306) until the sawtooth wave is fallen to the original state in

synchronization with the pulse signal outputted from the sawtooth wave discharging pulse circuit 40. At this time, the slope of the sawtooth wave becomes substantially zero.

In contrast, as shown in Fig. 6(E), in the case where the output current value of the constant current circuit 310 is smaller than the predetermined value, the slope of the sawtooth wave becomes smaller than the case mentioned above. Thus, the formed sawtooth wave becomes one having a gentle slope (small slope) because the capacitor 304 is not charged enough at the predetermined timing. In this case, since the height of the top of the sawtooth wave is low, this sawtooth wave is not suitable for the PWM control in which the sawtooth wave is compared with a predetermined voltage value to drive a load.

As shown in Fig. 6(F), in the condition that the slope of the sawtooth wave and the generation timing of the sawtooth wave discharging pulse are preferable, the sawtooth wave forming section 30 can output a clear and suitable sawtooth wave to the amplifier 50.

Next, a detailed description will be given for the relationship of output signals from the components in the sawtooth wave generating apparatus 1 with reference to the timing charts shown in Fig. 7. Fig. 7 shows timing charts schematically illustrating output signals from the voltage comparator 60 and the phase comparator 70, which correspond to enlarged view of the timing charts shown in Fig. 6.

In the timing charts shown in Fig. 7, from the top of the figure, an output signal from the base frequency generating section 10 (see Fig. 7(A)), an output signal from the frequency generating section 20 (i.e., the reference signal) (see Fig. 7(B)), an output signal from the sawtooth wave forming section 30 (i.e., the sawtooth wave output signal) (see Fig. 7(C)), an output signal from the voltage comparator 60 (see Fig. 7(D)), an output signal from the sawtooth wave discharging pulse circuit 40 (see Fig. 7(E)).

and an output signal from the phase comparator 70 (see Fig. 7(F)) are illustrated.

The reference line DAC shown in Fig. 7(C) indicates a reference voltage value inputted from the DAC 91 to the voltage comparator 60. When the output value of the sawtooth wave output signal is equal to the reference voltage value, the voltage comparator 60 outputs a pulse to the phase comparator 70 (see Fig. 7(D)). In synchronization with the pulse outputted from the voltage comparator 60, the sawtooth wave discharging pulse circuit 40 outputs a high-level signal, and keeps the high-level output for a predetermined time delayed by the delay circuit 402 (see Fig. 7(E)).

While the sawtooth wave discharging pulse circuit 40 outputs the high-level signal, the IGFET 305 in the sawtooth wave forming section 30 is turned on, whereby the electric charge stored in the capacitor 304 is rapidly discharged (see Fig. 7(C)).

In this regard, the time delayed by the delay circuit 402, i.e., the time when the output level of the sawtooth wave discharging pulse circuit 40 is high is appropriately set in consideration of the capacitance of the capacitor 304, the resistive value of the resistor 303, and the like.

Hereinafter, a description will be given for the operation of generating the sawtooth wave in the present embodiment according to the time series of the timing charts shown in Fig. 7.

The output signal from the base frequency generating section 10 is divided in the above-mentioned matter, thereby obtaining the output signal of the frequency generating section 20. The output signal from the frequency generating section 20 is a square-wave having a predetermined cycle (frequency) (see Fig. 7(B)). When the output value of the sawtooth wave output signal is equal to the reference voltage value of the DAC 91 (see Fig. 7(C)), the voltage comparator 60 outputs a pulse in timing with that time (see

Fig. 7(D)).

When the pulse signal of the voltage comparator 60 is inputted to the sawtooth wave discharging pulse circuit 40, the sawtooth wave discharging pulse circuit 40 outputs a high-level signal for a predetermined time from the timing of the pulse signal by the setting of the delay circuit 402.

At the same time, the phase comparator 70 compares the timing in which the pulse signal is outputted from the voltage comparator 60 with the timing of the rising edge of the square-wave, i.e., the output signal from the frequency generating section 20 (reference signal). In the first sawtooth wave output signal, since the output timing of the voltage comparator 60 is earlier than the rising timing of the reference signal, the phase comparator 70 outputs a low-level signal to the sawtooth wave forming section 30 via the LPF 80 for the time corresponding to the time difference so as to make the slope of the sawtooth wave ($\Delta V/t$) smaller, i.e., to reduce the amount of current flowing to the capacitor 304 (see Fig. 7(F)).

The voltage applied to the gate electrode of the first FET 301 is lowered by a predetermined value in response to the output signal from the LPF 80, thereby lowering the output current of the constant current circuit 310. Thus, as the second sawtooth wave shown in Fig. 7(C), the slope of the sawtooth wave, i.e., $\Delta V/t$ is made smaller, thereby delaying the timing in which the reference voltage signal of the DAC 91 is equal to the sawtooth wave output signal.

Similarly, as shown in Fig. 7(C), since the output timing of the voltage comparator 60 is also earlier than the rising timing of the reference signal of the frequency generating section 20 in the second sawtooth wave, the phase comparator 70 outputs the low-level signal to the sawtooth wave forming section 30 via the LPF 80 for the time corresponding to the time difference. Thus, the slope of the sawtooth wave is further made smaller, and the

timing in which the reference voltage signal of the DAC 91 is equal to the sawtooth wave output signal is further delayed.

In the third sawtooth wave, as mentioned above, by delaying the timing in which the reference voltage signal of the DAC 91 is equal to the sawtooth wave output signal, the rising timing of the reference signal of the frequency generating section 20 is earlier than the output timing of the voltage comparator 60 at this time. Therefore, to the contrary, the phase comparator 70 outputs a high-level signal for the time corresponding to the time difference (see Fig. 7(F)). Thus, the slope of the sawtooth wave is made larger, and the timing in which the reference voltage signal of the DAC 91 is equal to the sawtooth wave output signal is led.

Further, in the fourth sawtooth wave, to the contrary, since the output timing of the voltage comparator 60 is earlier than the rising timing of the reference signal of the frequency generating section 20, the phase comparator 70 outputs the low-level signal to the sawtooth wave forming section 30 via the LPF 80 for the time corresponding to the time difference. Thus, the slope of the sawtooth wave is made smaller, and the timing in which the reference voltage signal of the DAC 91 is equal to the sawtooth wave output signal is delayed.

Finally, in the fifth sawtooth wave, the rising timing of the reference signal of the frequency generating section 20 corresponds with the output timing of the voltage comparator 60. After this time, the sawtooth wave generating apparatus 1 (i.e., the sawtooth wave forming section 30) of the present invention can output (form) a good (clear) sawtooth wave output signal constantly unless disturbance or the like does not occur.

In this way, in the present invention, the reference signal having a given frequency is generated by the base frequency generating section 10 capable of generating the signal having a base frequency and the frequency generating section 20 capable of changing the base frequency of the output signal from the base

frequency generating section 10 into the given frequency, a sawtooth wave is formed in the sawtooth wave forming section 30 based on the generated reference signal, the phase of the top (apex) of the formed sawtooth wave is compared with the phase of the rising edge of the reference signal in the phase comparator 70, and the slope of the sawtooth wave, i.e., $\Delta V/t$ is automatically corrected based on the result of the phase comparison.

Further, in the step of automatically correcting the slope $\Delta V/t$, the pulse signal is generated in the voltage comparator 60 when the voltage value of the formed sawtooth wave reaches a predetermined voltage value, and the phase of the pulse signal is compared with the phase of the rising edge of the reference signal in the phase comparator 70. Then, in the case where the phase of the pulse signal is earlier than the phase of the rising edge of the reference signal, the amount of current flowing to the capacitor 304 is decreased by decreasing the gate voltage of the first FET 301, thereby making the slope of the sawtooth wave smaller. On the other hand, in the case where the phase of the pulse signal is later than the phase of the rising edge of the reference signal, the amount of current flowing to the capacitor 304 is increased by increasing the gate voltage of the first FET 301, thereby making the slope of the sawtooth wave larger.

As described above, in the sawtooth wave generating apparatus 1 and the method of generating the sawtooth wave in the above-described embodiment of the present invention, the slope of the formed sawtooth wave can be automatically adjusted by comparing the timing of the trailing edge of the sawtooth wave outputted from the sawtooth wave forming section 30, i.e., the timing in which the voltage comparator 60 outputs a pulse signal with the timing of the rising edge of the reference signal outputted from the frequency generating section 20 by means of the phase comparator 70, feeding back the predetermined signal to the sawtooth wave forming section 30 based on the result of the phase comparison, and adjusting the output current of the constant current circuit 310.

Therefore, according to the sawtooth wave generating apparatus 1 and the method of generating the sawtooth wave of the present invention, a sawtooth wave can be stably supplied (outputted) in response to variation in the resonant frequency of the resonant device (piezoelectric element) in the case of PWM-controlling a driving device with the piezoelectric element whose resonant frequency constantly undergoes a change, or carrying out the PWM control by arbitrarily changing the resonant frequency.

It should be noted that, in the embodiments described above, the case where the reference frequency of the signal outputted from the reference frequency generating section 102 is changed in response to the variation in the resonant frequency of the piezoelectric element is described, but the present invention is not limited to this case. It is also possible to apply the sawtooth wave generating apparatus and the method of generating the sawtooth wave to the case where a distortion or the like occurs in the sawtooth wave output signal outputted from the sawtooth wave forming section 30 due to some sort of disturbance.

Further, in the present embodiment, the frequency generating section 20 divides the frequency of the signal outputted from the base frequency generating section 10 using the H period forming section 201 and the L period forming section 202, but the present invention is not limited to this structure. The frequency generating section 20 may be constructed to use a divider or the like.

As described above, it should be noted that, even though the sawtooth wave generating apparatus and the constant current circuit according to the present invention have been described with reference to the preferred embodiments shown in the accompanying drawings, the present invention is not limited to these embodiments, it is of course possible to make various changes and modifications to each element of sawtooth wave generating apparatus and the

constant current circuit, and various elements described above can be replaced with any other element capable of performing the same or a similar function.